

Cenaero

BS1 - DNS of the transition of the Taylor-Green vortex, Re=1600

Introduction and result summary

Koen Hillewaert Fluid dynamics TL Contact: koen.hillewaert@cenaero.be

Testcase description Problem definition

Periodic domain

 $(x, y, z) \in \Omega = [-\pi L, \pi L]^3$ (x', y', z') = (x, y, z)/L

At t=0

$$u = V_0 \sin x' \cos y' \cos z'$$

 $v = -V_0 \cos x' \sin y' \cos z'$
 $w = 0$
 $p = p_0 + \rho_0 V_0^2 (\cos 2x' + \cos 2y') (\cos 2z' + 2) / 16$
 $T = T_0$

with

$$Re = \rho_0 V_0 L/\mu = 1600$$
$$M = V_0/\sqrt{\gamma R T_0} = 0.1$$

BS1 - Taylor-Green vortex Re=1600

van Rees et al., JCP 2011

© 2016 Cenaero - All rights reserved



Testcase description Problem definition

Periodic domain

 $(x, y, z) \in \Omega = [-\pi L, \pi L]^3$ (x', y', z') = (x, y, z)/L

At t=0 $u = V_0 \sin x' \cos y' \cos z'$ $v = -V_0 \cos x' \sin y' \cos z'$ w = 0 $p = p_0 + \rho_0 V_0^2 (\cos 2x' + \cos 2y') (\cos 2z' + 2) / 16$ $T = T_0$

with

$$Re = \rho_0 V_0 L/\mu = 1600$$
$$M = V_0/\sqrt{\gamma R T_0} = 0.1$$

BS1 - Taylor-Green vortex Re=1600

van Rees et al., JCP 2011

© 2016 Cenaero - All rights reserved



Testcase description Reference : pseudo-spectral 512 modes (courtesy UCLouvain)





Kinetic energy

$$E_k = \frac{1}{\rho_0} \int_{\Omega} \rho \, \frac{\mathbf{u} \cdot \mathbf{u}}{2} \, d\Omega$$

Dissipation rate and relation to enstrophy

$$\epsilon = -\frac{dE_k}{dt} = 2\frac{\mu}{\rho_0} \int_{\Omega} \mathbf{S}^d : \mathbf{S}^d \ d\Omega + \underbrace{\frac{\mu_v}{\rho_0} \int_{\Omega} (\nabla \cdot \mathbf{v})^2 \ d\Omega}_{\epsilon_2 \approx 0} - \underbrace{\frac{1}{\rho_0} \int_{\Omega} p \ \nabla \cdot \mathbf{v} \ d\Omega}_{\epsilon_3 \approx 0}$$

Testcase description Reference : pseudo-spectral 512 modes (courtesy UCLouvain)



Spectral convergence ~ 256³

Kinetic energy

$$E_k = \frac{1}{\rho_0} \int_{\Omega} \rho \, \frac{\mathbf{u} \cdot \mathbf{u}}{2} \, d\Omega$$

Dissipation rate and relation to enstrophy

$$\epsilon = -\frac{dE_k}{dt} = 2 \frac{\mu}{\rho_0} \int_{\Omega} \mathbf{S}^d : \mathbf{S}^d \ d\Omega + \underbrace{\frac{\mu_v}{\rho_0}}_{\epsilon_1 = 2\nu\mathcal{E}} \underbrace{\int_{\Omega} (\nabla \cdot \mathbf{v})^2 \ d\Omega}_{\epsilon_2 \approx 0} - \underbrace{\frac{1}{\rho_0} \int_{\Omega} p \ \nabla \cdot \mathbf{v} \ d\Omega}_{\epsilon_3 \approx 0}$$

C 2016 Cenaero - All rights reserved

Testcase description Reference : pseudo-spectral 512 modes (courtesy UCLouvain)



Kinetic energy

$$\mathsf{E}_k = \frac{1}{\rho_0} \int_{\Omega} \rho \, \frac{\mathbf{u} \cdot \mathbf{u}}{2} \, d\Omega \, ,$$

Dissipation rate and relation to enstrophy

 $\epsilon = -\frac{dE_k}{dt} = 2 \underbrace{\frac{\mu}{\rho_0} \int_{\Omega} \mathbf{S}^d : \mathbf{S}^d \ d\Omega}_{\epsilon_1 = 2\nu\mathcal{E}} + \underbrace{\frac{\mu_v}{\rho_0} \int_{\Omega} (\nabla \cdot \mathbf{v})^2 \ d\Omega}_{\epsilon_2 \approx 0} - \underbrace{\frac{1}{\rho_0} \int_{\Omega} p \ \nabla \cdot \mathbf{v} \ d\Omega}_{\epsilon_3 \approx 0}$

Cenae

Testcase description Error definitions

Errors with respect to pseudo spectral solution

$$\begin{split} \Delta \epsilon_1 &= \left| \left| \frac{dE_k}{dt} - \left(\frac{dEk}{dt} \right)^* \right| \right|_{t,\infty} \\ \Delta \epsilon_2 &= \left| \left| 2\nu \mathcal{E} - 2\nu \mathcal{E}^* \right| \right|_{t,\infty} \end{split}$$

Numerical dissipation : difference with DNS

$$\Delta \epsilon_3 = \left\| \left| \frac{dE_k}{dt} + 2\nu \mathcal{E} \right| \right|_{t,\infty}$$

with

$$||a||_{t,\infty} = \max_{t \in [0,10]} |a|$$

CPU time to reach $t_c = 10$, measured in WU



Testcase description Comparison of flow field at t=8





Cenaerd

- Y. Abe, I. Morinaka, T. Haga, T. Nonomura and K. Miyaji (JAXA) order convergence studies (1,3,7 and 15) on 128 mesh using SFFR with Roe and kinetic energy preserving flux (+ studies on unstructured meshes);
- M. Kupiainen, J. Nordström and P. Eliasson (LIU/SHMI/FOI) grid convergence studies (64/128/256) with SBP(84) scheme;
- M. Lorteau, M. de la Llave Plata, V.Couaillier (Onera) Aghora : grid convergence studies (64/128/256) with DGM at orders 2,3,4 and 5;
- A. Mastellone (CIRA) SparkLES : grid convergence studies (64/128/256) FVM 2nd and 4th order explicit, 4 and 6th order compact schemes;
- F. Navah and S. Nadarajah (McGill) : grid convergence studies (64/128/256) using CPR-DG(Roe/BR2) at interpolation orders 3,4,5 and 9;
- A. Nigro (UCalabria/UBergamo) grid convergence studies of DGM schemes Exp-ERS (explicit), Imp-ERS (Rosenbrock), Imp-pRoe (Rosenbrock, preconditioned Roe) at orders 1,2,3,4 and 5;
- A. West (CD-Adapco) : convergence studies (128/256) using FVM Upwind (2) and MUSCL-CD(3)
- J. Yu (BUAA) DGM studies 80/96/160 at orders 2,4;



Global results Error on measured dissipation : resolution



BS1 - Taylor-Green vortex Re=1600

© 2016 Cenaero - All rights reserved



Cenaero

Global results Error on measured dissipation : cpu time



BS1 - Taylor-Green vortex Re=1600

C 2016 Cenaero - All rights reserved

Global results Error on enstrophy dissipation : resolution



BS1 - Taylor-Green vortex Re=1600

C 2016 Cenaero - All rights reserved

Cenaero

Global results Error on enstrophy dissipation : cpu time



Global results Difference between measured and theoretical dissipation : resolution



BS1 - Taylor-Green vortex Re=1600

Global results Difference between measured and theoretical dissipation : cpu time



Conclusions

Cenae

- whatever method, 256 seems necessary to perform DNS, otherwise LES
- order of accuracy not obtained
- higher order at isodof pays off
- error on measured dissipation always lower than error on enstrophy and closer by for all methods and less dependent on order. Natural tendency of numerics to compensate lack of resolution?
- Kinetic energy preservation / central discretisation can be counterproductive, not only for measured dissipation but also for enstrophy; require SGS.
 - Abe : comparison Kep/Roe
 - High order FV (Cira)
 - SBP(84)
- not much impact of order on FVM schemes ??
- similar, but surprisingly not too close errors for DGM;
 - importance of flux function for DGM?
 - difference structured/unstructured mesh quite pronounced?
- difficult to measure efficiency. Eg. precision in dof compensated by speed for $\mathsf{FV}/\mathsf{Cira}$ \sim structured operator
- difference measured / theoretical dissipation good measure for precision order